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(54) APPARATUS FOR MEASURING SMALL DEVIATIONS FROM A TRUE HORIZONTAL PLANE

5 (71) We, ARTHUR D. LITTLE, INC., of 25 Acorn Park, Cambridge, Massachusetts, United States of America, a Corporation organised under the laws of the Commonwealth of Massachusetts, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly 10 described in and by the following statement:—

15 This invention relates to apparatus for measuring deviations from a true horizontal plane such as those deviations which may occur continuously or recurrently as a result of ground motion and the like.

20 By the term "true horizontal plane" used herein and in the claims is meant a plane which is exactly perpendicular to the local vertical direction such as defined for example by a plumb line. Thus, in effect, the apparatus measures the horizontal component of the acceleration of gravity. The magnitude of any such deviations to be measured may be extremely small, and the phenomena to be evaluated which bring about such deviations may have either very long periods or be aperiodic and proceed at very slow rates. Thus, such apparatus must 25 have reliable long-term stability. Instruments suitable for such measurements are generally referred to as "tiltmeters," and this generic term will be used hereinafter for convenience in describing the apparatus of this invention.

30 Tiltmeters have a number of different uses, and the following are given as examples of some of these. A tiltmeter may be used to determine the response of the ground or structure to loadings and hence to indicate the suitability of an area for heavy construction or the ability of a bridge to bear weight. They may be used to indicate the stability of foundations of buildings,

45 of dams, of slopes in open pit mining or of underground mining operations. Tiltmeters may also be employed in accurately positioning large scientific apparatus such as telescopes and particle accelerators. The property to measure the response of the ground to loads may also be used to determine the weight of large vehicles and the like.

50 55 One class of tiltmeters now in use depends upon measuring the change in level of water or mercury in a tube. All other presently available tiltmeters make use of a pendulous mass suspended on fine fibers or elastic hinges consisting of a thin strip of steel or similar metal. This latter class of instruments measures the displacement of the mass due to the acceleration or force required to restore the mass to its initial position. Because of material limitations which are inherent in the highly compliant suspension elements, they tend to be extremely fragile instruments and to be subjected to undesirable drifts in the zero point.

60 65 70 The present invention consists in an apparatus for measuring deviation from a true horizontal plane in which the movement of an elongated diamagnetic mass along its axis is detected by detecting means as a function of the inclination of the apparatus from said true horizontal plane, said elongated diamagnetic mass being levitated in a horizontal plane along its axis by magnetic field generating means, the flux concentration of said magnetic field being essentially symmetrical along the axis of said magnetic field being essentially symmetrical along the axis of said mass and exhibiting vertical and transverse gradients whereby said mass is strongly constrained transversely but is free to move axially. Any axial shift in the mass brought about through the effective tilting of the apparatus can be measured and used to deter-

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mine the actual tilt of the base and hence its deviation from the predetermined horizon. Some damping of the axial shift may be desirable, and means for accomplishing such damping may be provided as well as means for restoring the mass to a null position.

The invention also consists in a geo-physical instrument incorporating an apparatus as described above.

In order that the invention may be more readily understood, reference will now be made to the accompanying drawings in which:

15 Figs. 1 to 3 are diagrammatic cross sections through pole pieces of the tiltmeter of this invention showing three different configurations of the pole pieces and of the diamagnetic body serving as the mass;

20 Fig. 4 is a diagrammatic longitudinal cross section of the pole pieces of Fig. 1;

Figs. 5 and 6 are diagrammatic longitudinal cross sections of pole pieces showing modifications in pole piece construction 25 for limiting or restraining the axial motion of the diamagnetic mass;

30 Fig. 7 shows the use of electrically conducting caps on the diamagnetic mass for damping;

Fig. 8 is a cross section of the diamagnetic mass showing the use of a copper shield;

35 Fig. 9 is a perspective view of one embodiment of a tiltmeter constructed in accordance with this invention using a single permanent magnet and one form of detecting means;

40 Fig. 10 is a perspective view, partially cut away, of another embodiment of a tiltmeter constructed in accordance with this invention showing the use of two permanent magnets and another embodiment of detecting means;

45 Fig. 11 is a fragmentary cross section through the diamagnetic mass of the apparatus of Fig. 10;

50 Fig. 12 is a perspective view of an embodiment of the tiltmeter having yet another type of detecting means and incorporating means for controlling the environment around the magnetic field;

55 Fig. 13 is a circuit diagram for the readout and recording mechanism associated with the tiltmeter of Fig. 12;

Fig. 14 illustrates a modification of the field generating means of a tiltmeter constructed in accordance with this invention in which a series of magnets are used to generate eddy currents for damping;

60 Fig. 15 illustrates diagrammatically the magnetic fields and eddy currents developed in the arrangement of Fig. 14;

Fig. 16 is a circuit diagram of a tiltmeter using capacitors in the readout circuit;

65 Fig. 17 illustrates a tiltmeter which in-

corporates a zero-rebalance servo system; and

Fig. 18 illustrates another modification of the tiltmeter having a zero-rebalance system employing a capacitance displacement detection system.

The operation of the tiltmeter of this invention is illustrated in diagrammatic fashion in Figs. 1 to 4; while actual tiltmeter apparatus are shown in detail in Figs. 9 to 1—14. It will be appreciated that in Figs. 1 to 8 no attempt has been made to draw the component to scale and that the sizes of the various components have been somewhat enlarged for ease of illustration.

Fig. 1 illustrates how a mass of a diamagnetic material such as an elongated cylinder 20 may be suspended in a properly designed magnetic field 21. In order to achieve the desired levitation of the mass 20, it is necessary to provide a magnetic field which has a vertical gradient decreasing upwardly, as well as, symmetrical gradients transverse to the mass 20 which are substantially uniform along the axis of the mass. In Fig. 1 the lines of flux have been drawn in to illustrate the flux gradient, and from these lines it will become apparent that the magnet is so arranged as to

strongly constrain the diamagnetic mass in the transverse direction while leaving it free to move without friction in the axial direction. As will become apparent in the following detailed description, the axial movement is measured and used as a means for evaluating deviation of the suspended mass from the true horizontal plane.

The desired magnetic field is achieved by use of an upper pole piece 25 in which there is a groove 26 having edges 27 and 28 which, according to well-known physical principles, effects a concentration of the magnetic flux. A lower pole piece 29 is provided and in the construction of Fig. 1 is seen to terminate in a narrow, flat surface 30, which provides edges 31 and 32 aligned with edges 27 and 28 to achieve the desired lateral flux gradient as well as the vertical gradient. It will be appreciated that these edges need not be sharp but may be rounded to optimize magnetic saturation in the pole-piece material.

Fig. 2 shows a modification of the basic arrangement of Fig. 1 and illustrates the use of a triangularly shaped diamagnetic mass 35. In this modification, in which like numbers refer to like elements, the bottom pole piece terminates in a single edge 36 which is symmetrically positioned with respect to edges 27 and 28 of upper pole piece 25.

Fig. 3 illustrates yet another modification of the pole piece configurations as well as the use of a rectangularly shaped diamagnetic mass 39. In the arrangement of Fig. 130

3, the upper pole piece 41 has a groove 26, which is cut in a stepped configuration which presents a second pair of flux concentrating edges 42 and 43. The lower pole 5 piece is provided in the form of symmetrical halves 44 and 45, the edges of which are aligned with edges 27 and 28. The lower pole pieces are positioned in spaced relationship to define a narrow passage 46 between them.

10 The mass when formed of a diamagnetic material may be levitated in the manner illustrated in Figs. 1 to 3 provided certain requirements are met. The condition of 15 levitation in a magnetic field may be written as

$$\frac{1}{2} \nabla \bar{H}^2 - \frac{\rho g}{|x|} = 0$$

20 where the average of \bar{H}^2 is taken over the volume of the suspended body, H being the magnetic field strength, χ is its diamagnetic susceptibility, ρ its density, and g is the acceleration of gravity. Thus, the magnetic field must be of sufficient strength to overcome the gravitational force exerted on the 25 diamagnetic mass. In practice, the value of

30 \bar{H}^2 is limited by the size and the energy product $(BH)_{max}$ of the magnet, B being the magnetic induction of the material. It is also, of course, desirable to use a material 35 for the mass which has the lowest possible value of ρ/χ . Pure graphite has been found to be the best diamagnetic material for the mass, although other materials may be used. These other materials include, but 40 are not limited to, fused quartz, boron, beryllium, and certain other metals, glasses and liquids, the latter being contained within suitable tubing. It is, of course, well known that a superconductor has the highest value 45 of diamagnetic susceptibility, and it is within the scope of this invention to employ a superconducting mass and provide means for maintaining the tiltmeter at a temperature sufficiently low to maintain the mass superconducting.

50 The actual size of the diamagnetic mass will, of course, depend upon the size of the magnet or magnets used and the magnetic properties of the pole pieces as well as the diamagnetic susceptibility of the mass. As an example, tiltmeters have been constructed as shown in Figs. 9 and 10 using graphite rods one-tenth inch in diameter and about one inch long as the diamagnetic 55 mass and a horseshoe shaped magnet having an overall length of approximately three inches and a volume ranging between two and four cubic inches.

60 It will be seen from Fig. 4, which is a longitudinal cross section of the arrangement of Fig. 1, that the two ends 51 and

52 of the gap defined by the pole pieces 25 and 29 in which the magnetic field is established are so constructed as to offer no constraining forces to the axial movement 65 of the suspended mass 20. Thus, in such an arrangement without any axial constraints, the mass may be shifted far enough to one side or the other to enter an unstable condition and escape by one or the other end. 70 It is, therefore, necessary that some means be provided to provide at least a slight constraining force along the axis of the diamagnetic mass to restore it to a null or central position. A number of axial constraining and restoring means are available. 75 Figs. 5 and 6 illustrate modifications in the configurations of the pole pieces to achieve axial constraint and restoration. Figs. 7 and 8 illustrate modifications in the construction of the diamagnetic mass to accomplish damping of the axial motion of the diamagnetic mass through the use of 80 eddy currents.

Once the suspended mass has moved in 85 the axial direction and its motion detected and recorded, it is necessary that its further motion be limited by a force equal and opposite in direction to that resulting from the tilt. It is also necessary to constrain 90 its axial motion within certain limits to permit this restoration. Such constraining and restoring means must be capable of opposing the axial motion of the suspended mass and of providing a force proportional 95 to the displacement of the mass. Two modifications in pole piece configurations to provide the required constraining and restoring forces are illustrated in Figs. 5 and 6.

100 In Fig. 5 the lower pole piece 55 is modified such that the ends are higher and hence closer to edges 27 and 28 than is the edge or edges along the central portion of the pole. This then establishes a magnetic flux 105 gradient in which the strongest flux exists at the ends 56 and 57. Therefore, as the mass 20 shifts from its central position to either the left or the right, it encounters stronger magnetic fields, its axial movement is opposed, and the mass is constrained within the gap defined by the pole pieces 110 and restored to a central position.

115 In Fig. 6 the upper and lower pole pieces 59 and 60 are cut such that they are in effect concave which brings about a more gradual change of the flux gradient between the ends 61 and 62 and hence effects a more uniform restoring force acting on the mass. Ideally, the concave shape of the 120 pole pieces should be designed to cause the restoring force to increase proportionally with the displacement of the diamagnetic mass from its initial position.

125 It is also necessary to provide suitable damping means which in effect provide a

dragging force which opposes the motion of the suspended mass and which is proportional to the velocity of the axial motion. In contrast to the constraining and restoring forces which effect a conservation of energy, the damping forces effect a dissipation of energy in the form of heat.

Figs. 7 and 8 illustrate modifications which may be made on the suspended mass 20 to achieve the required damping through the use of eddy currents. In Fig. 7 the mass is seen to have thin caps 65 and 66 on each end formed of an electrically conducting, nonmagnetic material such as aluminum or copper. Alternatively, the entire mass 20 may be encased in an electrically conducting material 67 as illustrated in Fig. 8. Such damping means are used in the tiltmeter modifications shown in Figs. 10 and 14; while Fig. 9 illustrates the use of an external magnetic field for damping. The manner in which these damping means function will be described in detail in the discussion of the various embodiments and modifications of the tiltmeter.

A tiltmeter constructed in accordance with this invention is illustrated in detail in Fig. 9. There is provided a permanent horseshoe magnet 75 having a north pole 76 and a south pole 77. In keeping with well-known practice, an upper pole piece 78, formed of a highly magnetically permeable material such as soft iron or iron-cobalt alloy, is affixed to the upper pole, and a suitably shaped lower pole piece 79, also formed of a highly permeable material, is affixed to the south pole to achieve the desired gap configuration to define the magnetic field 21 as shown in cross section in Fig. 1. An elongated cylindrical piece of graphite 80 serves as the diamagnetic mass. Light-weight rods 84 and 85 (formed of a non-magnetic material such as aluminum) are affixed to the two ends of the mass 80. On rod 85 is attached a light-weight vane 86, formed of aluminum or other non-magnetic material, which is held in position in the gap of a small auxiliary magnet 87 to serve as a damping means to slow down the axial movement of mass 80. On the other end of the mass 80 is positioned a means for detecting axial movement of the mass. This comprises a thin vane 90 (e.g., of aluminum) of a weight equal to that of the vane 86. A narrow slit 91 is cut in vane 90. Light from a suitable source such as light bulb 94 is directed by means of lens 95 onto slit 91; and that light which passes through slit 91 is collected by means of lens 96 to be directed onto a differential photoresistor device 97 which has two photo-sensitive cells 98 and 99. A dc current is supplied to the cells from a suitable source such as battery 102, and each of the cells has associated with it a resistor 103 and

104; and a millivoltmeter 105, or other differential signal detecting means, is placed in the circuit.

In the absence of any axial movement of the mass 80, i.e., when the mass is in its null position, light from source 94 passing through slit 91 is made to fall equally on cells 98 and 99, and the millivoltmeter 105 reads zero. When, however, the mass moves in an axial direction, the position of slit 91 is altered with respect to cells 98 and 99, thus shifting the balance within the differential photoresistor and hence within the resistors 103-104. This shift in balance is registered on millivoltmeter 105 as a measure of the axial movement of the mass.

Figs. 10 and 11 illustrate another modification of the tiltmeter of this invention. In this modification two permanent magnets 110 and 111 are provided, and the two north poles 112 and 113 are affixed to a common upper pole piece 114 while the two south poles 115 and 116 are affixed to a common lower pole piece 117. The magnetic field 21, defined by the gap between the two pole pieces, is effectively closed in by means of the end pieces 120 and 121 typically constructed of soft iron or an iron-cobalt alloy.

In the tiltmeter of Figs. 10 and 11, the mass is seen to be a long cylinder of graphite 125 covered throughout its length with a thin copper sheath 126 to achieve eddy current damping.

Axial movement of the mass of Figs. 10 and 11 is detected optically. Mounted on either side of the central section of the mass are small light-weight vanes 130 and 131 (see Fig. 11). These are positioned so that the edges of the vanes coincide with the opposite edges of two staggered photoresistive light sensors 132 or 133. These sensors are so positioned that the sensor 132 on the left side (Fig. 11) is adapted to detect said axial motion in the direction of the arrow associated with vane 130; while the sensor on the right side is adapted to detect axial motion in the direction of the arrow associated with vane 131. The light sensors are positioned within channels 134 and 135 drilled on either side of the lower pole piece 117, and suitable leads from these sensors 136 and 138 are provided for connection to an external circuit suitable for detecting the amount of radiant energy reaching the sensors 132 and 133. Such a circuit is shown in Fig. 13 and described below in detail.

Light is provided to the detecting system 125 of Fig. 10 by means of two small radiant energy sources such as light bulbs 150 and 151 positioned within channels 152 and 153 drilled in the upper pole piece. It will, of course, be obvious to those skilled in the

art that a single source of radiant energy may be used rather than the two separate sources of Fig. 10. Thus, the beam from a single source may be split using well-known optical elements, e.g., mirrors, and the two beams directed into channels 152 and 153. Smaller diameter channels such as 155 shown in Fig. 10 communicate with the larger channels containing the light source and are so aligned as to direct light onto the sensors 132 and 133 as the vanes move axially.

When the tiltmeter is in its null or normal position, vanes 130 and 131 will just completely cover the sensors 132 and 133. With any axial movement, however, one of these sensors is uncovered, and the differential voltage produced by the imbalance of their output becomes a measurement of the movement of the vane and hence of the mass 125.

In the modification of the tiltmeter shown in Figs. 12 and 13, another means for detecting axial motion of the diamagnetic mass is shown. Means are also provided for controlling the atmosphere around the pole pieces, the mass, and a portion of the detecting elements. The primary purpose for controlling the atmosphere around the mass is to minimize the effects of ambient temperature fluctuations, eliminate dust and convective air currents as well as to control precisely the amount of radiant energy reaching the detecting system.

In the embodiment of Fig. 12 the desired magnetic field is obtained through the use of a single permanent magnet 160, the north pole 161 of which is affixed to a suitable contoured upper pole piece 162 and the south pole 163 to a lower pole piece 164. The magnet 160 is attached to a vertical support 168, which may be made integral with a base 169. The base, and hence the tiltmeter, is leveled by means of two screws 170 (one which is shown) and a fine adjustment screw 171.

In the modification of Fig. 12, the diamagnetic mass 175 is seen to extend beyond the confines of the gap defined between the two pole pieces, and on the ends of the seismic mass are hung light-weight vanes 176 and 177 preferably made of aluminum foil. These vanes are positioned such that the outer edge is aligned with an associated photodiode 178 and 179 of the silicon n-p-n type.

A light source 183 is provided, and two concave mirrors 184 and 185 are placed diametrically opposite to the light source to project two separate beams of light, which are alternately obstructed by the vanes attached to the seismic mass. The focal length of the mirrors is such as to form two equally bright images of the light source filament on the two photodiodes. As will

be seen in Fig. 13, the photodiodes 178 and 179 are connected in a circuit supplied from a precision regulated power source 186 and including a differential amplifier 187 which in turn may be connected through switch 188 to a microammeter 189, to a chart recording self-balancing potentiometer 190 or to both these output detecting devices. Power is supplied to the light source 183 from any suitable power source 191. Alternatively, the precision regulated power source 186 may supply power to the light source 183 as well as to the diodes. Regulation better than 0.01 percent line and load voltage variation in the power source 186 must be provided to operate the device. The bridge output is typically of the order of 100 mv (with a 10,000 ohm load) for a 0.1 mm displacement of the diamagnetic mass.

Since it is desirable to protect the diamagnetic mass and the detecting system from atmospheric convections, ambient light and dust and external magnetic fields, enclosure 193 is positioned around the mass, the radiant energy source and optical elements of the detecting means. The enclosure is made of any suitable nonmagnetic material, and if it is made fluid-tight, it is possible to introduce into the enclosure through a suitably valved conduit 194 a fluid to surround the mass. Thus, for example, a fluid of proper viscosity may be used to provide the necessary damping forces to oppose the motion of mass 175.

Although damping may be achieved through the use of a viscous fluid, it is preferably accomplished through the establishment of suitable eddy currents. In order to make the eddy current damping sufficiently strong, the diamagnetic mass must exhibit good electrical conductivity. If the mass were made of beryllium, for example, it is possible that the conductivity of this metal might be satisfactory for the purpose. However, in the case of graphite, the conductivity is much lower and the induced eddy currents in a graphite mass are not strong enough to cause effective damping. Therefore, it is necessary to enhance its electrical conducting properties. This can be done most conveniently by attaching to the diamagnetic mass an electrically conducting, nonmagnetic member or members such as the end caps 65 and 66 of Fig. 7 or the enclosing sheath 67 of Fig. 8. Such members are preferably formed of aluminum or copper. As the mass with the electrically conducting member moves through the nonuniform magnetic field, an electrical current is induced within the conducting member and the current circulates in a manner as to oppose the motion of the conductor and hence the diamagnetic body with which it is associated. Thus, the axial

motion of the mass is damped by the opposing force.

The configuration shown in Fig. 14 is designed to achieve an improved form of 5 eddy current damping. In the arrangement of Fig. 14, the eddy currents are induced in a copper sheathed diamagnetic mass 204 as it moves along the axis. This is achieved by using a plurality of identical magnets 10 200 with nonmagnetic spacers 203 retaining them in spaced relationship. The magnets are so arranged as to alternate polarity, and the upper pole piece 201 and lower pole piece 202 are constructed of contoured elements in accordance with the requirements 15 of the invention. The nonmagnetic spacers 203 are of such a thickness that the magnetic leakage flux between the magnets of opposed polarity does not substantially detract from the flux in the working gap. As 20 the diamagnetic mass 204 moves along its axis, the volume elements located between the adjacent magnets will see a reversal of flux and, consequently, eddy currents will be induced in them as shown schematically in 25 Fig. 15.

Fig. 26 illustrates another embodiment of displacement detection and readout which is based upon capacitance measurement 30 rather than upon electro-optical effects. In the arrangement of Fig. 16, the mass 210, which may be covered with a copper sheath 211, is positioned within a plurality of cylindrical electrodes 212_a to 212_e, located 35 within the gap defined by a north pole 213 and a south pole 214 constructed in accordance with the requirements discussed previously. The electrode 212_a at the extreme 40 right end of the electrode 212_e at the extreme left end of the electrode 212_e are electrically insulated from the remaining electrodes located between them, and they are interconnected with capacitors 215 and 216 forming a capacitance bridge 45 circuit 217, which is supplied with ac power from a suitable ac power source such as 218 operating in the audio or radio frequency range. When the electrically conducting mass 210 is centered between the 50 electrodes in its null position, the stray capacitances 221 and 222 are equal, the bridge 217 is balanced, and no voltage is recorded by millivoltmeter 233. The connection between the mass and the inner electrodes, which are grounded by ground 55 227, is provided by the inherent capacitances 225. Any axial movement of mass 210 is reflected by a change in the stray capacitances and is detected on millivoltmeter 223.

60 The magnets shown in the drawings of the various embodiments and modifications of this device have been illustrated as permanent magnets. It is, of course, within the scope of this invention to use electromagnets in place of the permanent magnets

shown, and such interchange is within the knowledge of one skilled in the art.

Fig. 17 shows the tiltmeter equipped with a zero-rebalance servo system which automatically forces the suspended diamagnetic mass back to the position of initial zero after the instrument has been tilted. The advantage of such a system is that it greatly increases the range over which tilts can be measured, all the way from a fraction of a second of arc to a few degrees. Embodied in the device of Fig. 17 is a modification of the magnet pole pieces which permits the axial gradient of the magnetic field to be made stronger or weaker at will by a dc control current.

In the device of Fig. 17, the optical portion of the detecting means is essentially that of Fig. 12 and includes a radiant energy source 183 and two mirrors 184 and 185 aligned with photocells 230 and 231 and the aluminum caps 232 and 233 affixed to the ends of a graphite cylinder 234 serving as the diamagnetic mass. The lower pole piece 235 is modified at either end to include electromagnets 236 and 237 having coils 238 and 239, respectively. In like manner, the upper pole piece 240 may be so modified to include electromagnets in addition to or in place of the electromagnets 236 and 237 associated with the lower pole piece.

Coil 238 is connected to a circuit which includes a current amplifier 242 and resistor 243; and in like manner, coil 239 is part of 100 a circuit including current amplifier 244 and resistor 245. Photocell 230 is connected to a differential amplifier 246 which has a feedback loop comprising capacitor 247 and resistor 248 in parallel; and photocell 231 is connected to a differential amplifier 250 which has a feedback loop comprising capacitor 241 and resistor 252 in parallel. It will be seen that differential amplifier 246 is also connected to current amplifier 110 244 and coil 239; while differential amplifier 250 is connected to current amplifier 242 and coil 238, the connections between the differential amplifiers and the coils providing current feedback loops. A dc current is provided to the amplifiers in the usual manner from a source not shown.

In the operation of the tiltmeter of Fig. 17, currents are passed through both coils 238 and 239 in a direction such as to reinforce the fields generated by the permanent magnets associated with the pole pieces. The fields at the ends of the pole pieces are thus made stronger similar to the situation shown in Figs. 5 and 6. Now, if one of 125 the currents in either coil 238 or 239 is made stronger, the stronger field generated by the corresponding electromagnet will push the diamagnetic mass toward the center of the suspension; similarly, making 130

the current which will permit the diamagnetic mass to move outwards, away from the center.

If the instrument is tilted so that the mass 234 shifts, say, to the right, the left-hand photocell 231 receives more light, and the left-hand differential amplifier 250 generates larger output voltage. This voltage is fed into the right-hand current amplifier 242 causing it to pass stronger current through the coil 238 on the right and the mass is forced to the left, back to the initial zero position. The current feedback loop delivers a voltage proportional to the restoring current to the other input of left-hand differential amplifier 250 and causes the mass promptly to reach the initial zero position to be held there as long as the instrument remains tilted. The purpose of the feedback loops associated with the differential amplifiers is to make the servo system more stable and less sensitive to rapid fluctuations. It is therefore preferred that the resistors 248 and 252 and capacitors 247 and 251 have suitably long-time constants. It is apparent that this action is reinforced by the symmetrically corresponding other half of the circuit. The actual tilt is measured by the strength of the current passing through either coil at balance and indicated by a milliammeter 254.

In Fig. 18 there is another kind of zero-rebalance system shown which employs the capacitance displacement detection system described earlier in conjunction with Fig. 16. The force acting upon the mass according to the system shown in Fig. 18 is of electrostatic nature rather than of magnetic nature as illustrated in Fig. 17. This force results from applying a voltage to an electrode located near the end of the suspended mass.

In the arrangement of Fig. 18 two pole pieces 256 and 257, designed according to Fig. 6, define the magnetic gap with the desired flux pattern, and a copper-sheathed graphite rod 258 serves as the diamagnetic mass. Interposed between the mass and the pole pieces are two end cylindrical electrodes 259 and 260 and a central electrode 261, this last electrode being connected to ground 262. Electrostatic forcer electrodes 263 and 264 are positioned within the terminal electrodes 259 and 260, and they are made part of zero-rebalance servo system which functions similarly to that of Fig. 17. This servo system is comprised of an ac source 265 and a capacitor 266 and differential amplifier 267 associated with terminal electrode 259; and of a capacitor 268 and differential amplifier 269 associated with terminal electrode 260. The differential amplifiers 267 and 269 are provided with feedback loops comprising resistors 270 and 271 and capacitors 272 and 273 in parallel which have suitably long-time constants as in Fig. 17.

The charged electrodes 263 and 264 of whatever polarity will induce charges of equal size and opposite polarity on the surface to the electrodes. Thus, the charging of one of the electrodes will cause the mass 258 to be attracted to that electrode. In this way it is possible to exert force on the mass in order to counteract its displacement caused by tilting the instrument. This electrostatic forcing system is, as indicated above, made a part of a zero-rebalance servo system. Since the displacement detection system employs ac current rather than dc, the imbalance in voltage in either side of the system is rectified by diodes 275 and 276 before it is applied to the input of the corresponding differential amplifier. In the feedback loops of this system, the feedback voltages are derived from resistive voltage dividers 277 and 278 connected to control electrodes 263 and 264; and voltage amplifiers 279 and 280 are provided in the electrostatic forcer electrode circuits. A millivoltmeter 281 is illustrated as representative of means for reading out the axial movement of the diamagnetic mass.

It is obvious that components of the systems shown in Figs. 17 and 18 may be interchanged so that, for example, the photoelectric displacement sensor is combined with the electrostatic forcing system, or the capacitance displacement sensor is used in connection with the electromagnetic forcer. It is also within the scope of this invention to incorporate into the devices of Figs. 16, 17, and 18 any suitable readout and recording means as illustrated in Fig. 13.

It is also understood that any of the embodiments and modifications of the tiltmeter of this invention may be constructed to have pole pieces of the various configurations illustrated in Figs. 1 to 6 and diamagnetic masses in any of the forms illustrated. Moreover, any other configurations for the pole pieces and/or diamagnetic mass which achieves the necessary radial constraint of the mass while permitting its desired controlled axial movement may be used.

The tiltmeters described above eliminate or reduce the drawbacks associated with the prior art devices by the use of a diamagnetic mass which is suspended in a magnetic field in which the normal elastic forces are replaced by field forces. The mass is, therefore, free to respond to accelerations without any trace of friction of external or internal origin. The absence of friction makes it possible to construct the instrument so that it is highly responsive while remaining relatively rugged. Moreover, when the instrument is constructed properly, it can be made to remain highly stable

over indefinite periods of time within reasonable limits of environmental variables.

WHAT WE CLAIM IS:—

1. An apparatus for measuring deviation 5 from a true horizontal plane in which the movement of an elongated diamagnetic mass along its axis is detected by detecting means as a function of the inclination of the apparatus from said true horizontal plane, 10 said elongated diamagnetic mass being levitated in a horizontal plane along its axis by magnetic field generating means, the flux concentration of said magnetic field being essentially symmetrical along the axis of 15 said mass and exhibiting vertical and transverse gradients whereby said mass is strongly constrained transversely but is free to move axially.
2. An apparatus as claimed in claim 1, 20 wherein said magnetic field generating means comprises at least one permanent magnet.
3. An apparatus as claimed in claim 1, 25 wherein said magnetic field generating means comprises a plurality of magnets arranged to alternate polarity and maintained in spaced relationship by nonmagnetic spacer means.
4. An apparatus as claimed in claim 1, 30 wherein said magnetic field generating means includes an upper pole piece defining a horizontal channel and a lower pole piece of a configuration to define with said upper pole piece said magnetic field.
5. An apparatus as claimed in claim 4, 35 wherein at least one of said pole pieces is contoured such that the distance between said pole pieces decreases at the ends thereof thereby to provide a restoring force.
6. An apparatus as claimed in claim 4, 40 wherein said pole pieces are concave in configuration.
7. An apparatus as claimed in any one 45 of the preceding claims, wherein said magnetic field generating means comprises a plurality of magnets arranged to alternate polarity and maintained in spaced relationship by non-magnetic spacer means.
8. An apparatus as claimed in any one 50 of the preceding claims, wherein said diamagnetic mass is formed of graphite.
9. An apparatus as claimed in any one 55 of the preceding claims, wherein said diamagnetic mass has associated therewith non-magnetic electrically conducting means serving as said means for damping said axial movement of said mass.
10. An apparatus as claimed in claim 9, 60 wherein said nonmagnetic electrically conducting means are metallic end caps attached to said diamagnetic mass and extending beyond the ends of said pole pieces.
11. An apparatus as claimed in claim 9, 65 wherein said nonmagnetic electrically con-

ducting means is a metallic sheath surrounding said diamagnetic mass.

12. An apparatus as claimed in claim 1 having means for damping the axial movement of said mass.
13. An apparatus as claimed in claim 120, wherein said means for damping said axial movement of said mass comprises an electrically conducting nonmagnetic member affixed to one end of said diamagnetic mass and means for providing a magnetic field around said mass, whereby axial movement of said mass effects movement of said member in said magnetic field to generate eddy currents.
14. An apparatus as claimed in any one 80 of the preceding claims having zero-rebalancing servo system means.
15. An apparatus as claimed in any one 85 of the preceding claims having enclosure means surrounding said diamagnetic mass and at least a portion of said means for detecting axial movement of said mass.
16. An apparatus as claimed in claim 1, 90 wherein said means for detecting axial movement of said mass comprises, in combination radiant energy source means, duplicate radiant energy responsive means adapted to generate signals proportional to radiant energy transmitted thereto from said source means, means associated with said diamagnetic mass, movable therewith and being adapted to control the quantity of said radiant energy transmitted to each of said radiant energy responsive means, and means adapted to receive said signals from 100 said radiant energy responsive means and to produce a detectable signal which is a function of the difference between said signals received from said radiant energy responsive means.
17. An apparatus as claimed in claim 16, wherein said means associated with said diamagnetic mass comprises a vane member having a slit therein and being attached to one end of said mass.
18. An apparatus as claimed in claim 16, wherein said means associated with said diamagnetic mass comprises two vane members positioned centrally on opposite sides of said mass and in staggered relationship 115 to each other whereby any movement of said mass causes one of said vanes to permit said radiant energy to be transmitted to its corresponding radiant energy responsive means.
19. An apparatus as claimed in claim 16, wherein said means associated with said diamagnetic mass comprises a vane member affixed to each end of said mass.
20. An apparatus as claimed in claim 1 120 having means for providing a restoring force to said diamagnetic mass.
21. An apparatus as claimed in claim 20, wherein said means for providing a

restoring force, said diamagnetic mass comprising electromagnets associated with the ends of at least one of said pole pieces.

22. An apparatus as claimed in any one of the preceding claims having readout means associated with said detecting means.

23. An apparatus as claimed in claim 4 having a plurality of annular cylindrical, nonmagnetic electrodes interposed in spaced relationship between said pole pieces and said diamagnetic mass, the two terminal electrodes of which extend beyond the ends of said mass, means for supplying electrical energy to said terminal electrodes thereby to establish capacitances between said ends of said mass and said terminal electrodes to serve as means for weakly constraining said axial movement of said mass and for restoring said mass to a null position, and means for detecting the difference between the magnitudes of said capacitances as a function of said axial movement of said mass.

24. An apparatus as claimed in claim 25, including zero-rebalance servo means associated with said means for detecting the difference between the magnitudes of said capacitances.

25. An apparatus as claimed in claim 30, 4 having first and second duplicate force applying means at the ends of said pole pieces adapted to return said diamagnetic mass to its central position subsequent to its axial movement, first and second duplicate energy source means associated with said first and second force applying means, respectively, first and second duplicate energy detecting means for detecting said axial movement, including differential amplifier means, said first energy source means being connected in responsive relationship to said second energy detecting means and said second energy source means being connected in responsive relationship to said first energy detecting means whereby the force applied by the one of said force applying means at the end of said pole pieces toward which said mass moves is increased and said mass is restored to its central null position, and means for detecting the difference of the forces applied as a function of said axial movement of said mass.

26. An apparatus as claimed in claim 55, wherein said force applying means are electromagnets and said source means are coils.

27. An apparatus as claimed in claim 25, wherein said force applying means are electrostatic force electrodes.

28. An apparatus as claimed in claim 4 having duplicate electromagnets positioned at the ends of at least one of said pole pieces, each of said electromagnets having a coil associated therewith, radiant energy source means, duplicate radiant energy responsive means, each of which is adapted to generate signals proportional to radiant energy transmitted thereto from said source means and positioned with respect to said mass so that said axial movement of said mass controls the amount of said radiant energy transmitted to each of said radiant energy responsive means, duplicate differential amplifier means, each of which is adapted to be responsive to signals received from a corresponding associated radiant energy responsive means, duplicate current amplifier means, each of which is arranged to supply current to its associated coil and is connected to the one of said differential amplifier means responsive to signals received from the opposite radiant energy responsive means, whereby the magnetic field is increased at that end of said pole pieces toward which said mass moves, thus providing an axially restoring force, and means for detecting the amount of current supplied to effect said restoring force.

29. An apparatus as claimed in claim 4 having a plurality of annular cylindrical, nonmagnetic electrodes interposed in spaced relationship between said pole pieces and said diamagnetic mass, the two terminal electrodes of which extend beyond the ends of said mass, first and second electrostatic force electrodes facing the ends of said mass, spaced therefrom and located within said terminal electrodes, first and second means for supplying electrical energy to said terminal electrodes thereby to establish capacitances between said ends of said mass and said terminal electrodes, the capacitances being proportional to said axial movement of said mass, first and second means for detecting said capacitances, and first and second means for supplying electrical energy to said electrostatic force electrodes, said first means being connected to said second means for detecting said capacitance and said second means being connected to said first means for detecting said capacitance whereby there is formed a zero-balanced servo means adapted to restore said mass to a central null position subsequent to its axial movement.

30. Apparatus for measuring deviation from a true horizontal plane, constructed, arranged and adapted to operate substantially as hereinbefore described with reference to the accompanying drawings.

31. A geophysical instrument incorporating apparatus as claimed in any preceding claim.

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16 Kensington Square,
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Chartered Patent Agents.

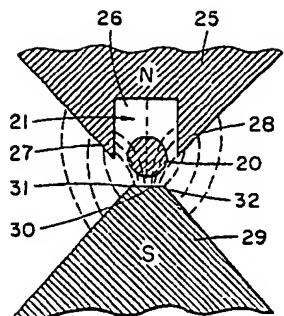


Fig. 1

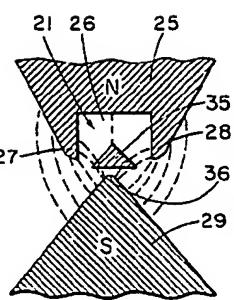


Fig. 2

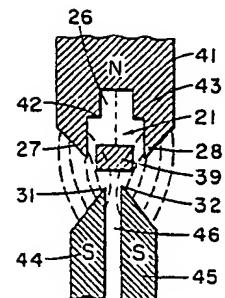


Fig. 3

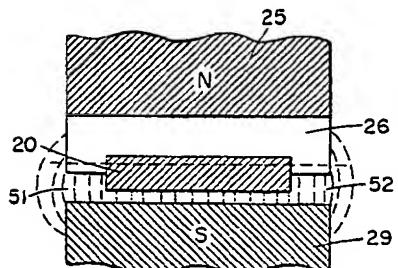


Fig. 4

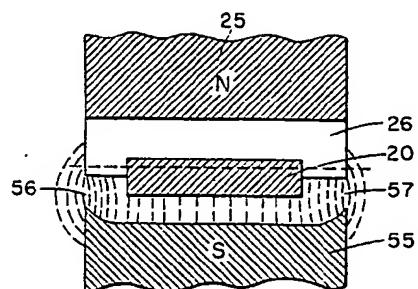


Fig. 5

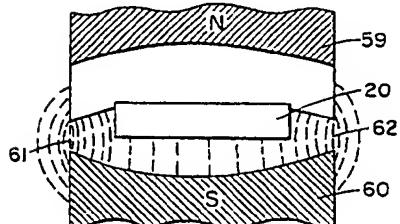


Fig. 6

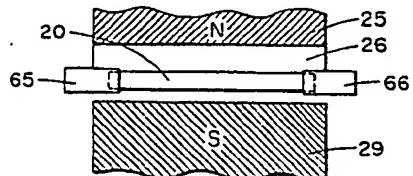


Fig. 7



Fig. 8

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6 SHEETS

COMPLETE SPECIFICATION

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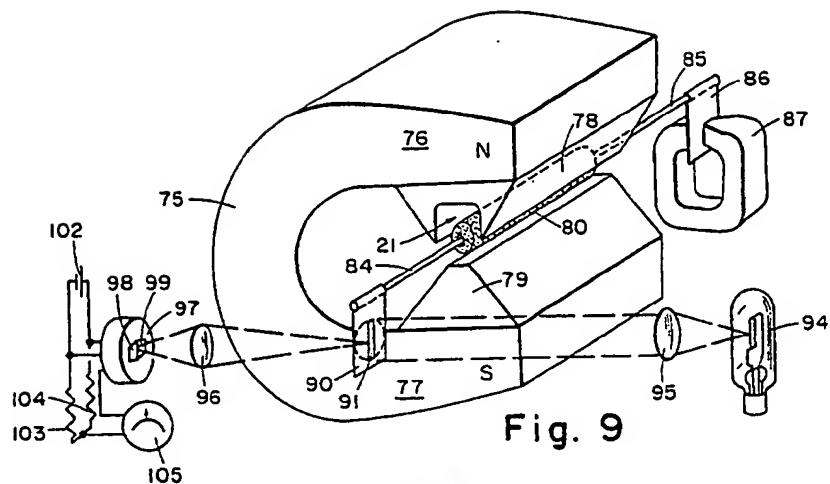


Fig. 9

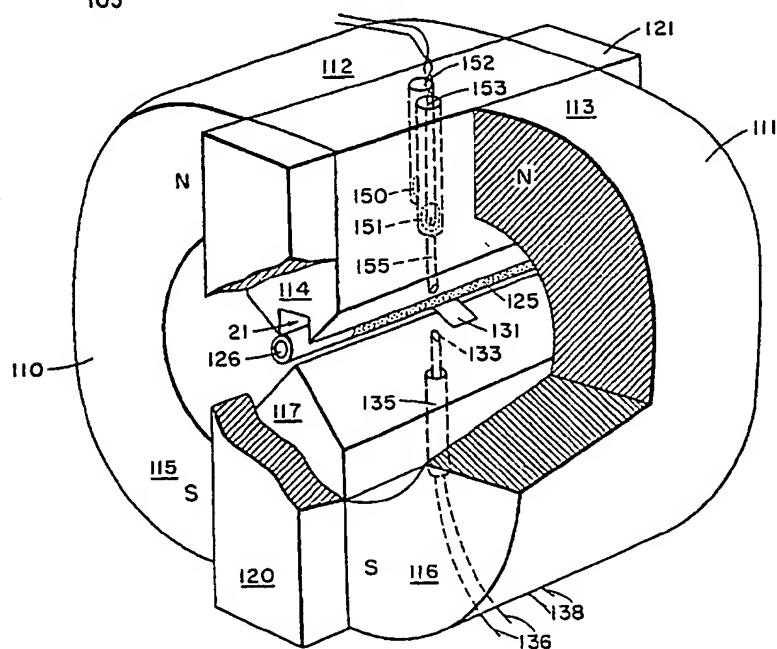


Fig. 10

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CONCRETE SPECIFICATION

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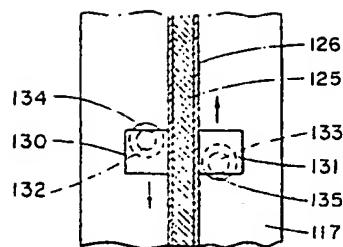


Fig. 11

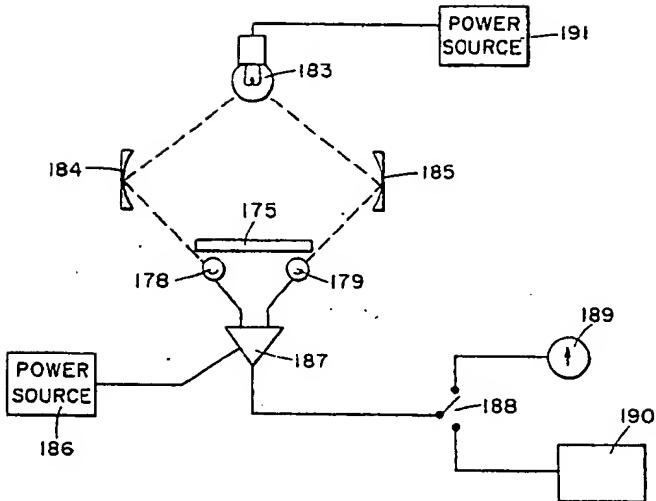


Fig. 13

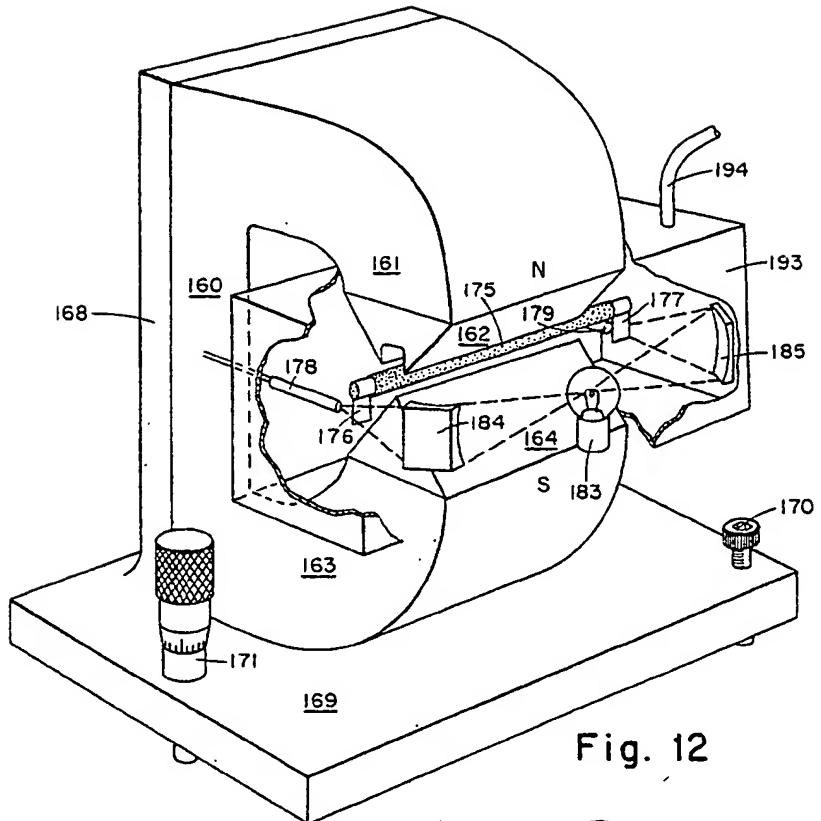


Fig. 12

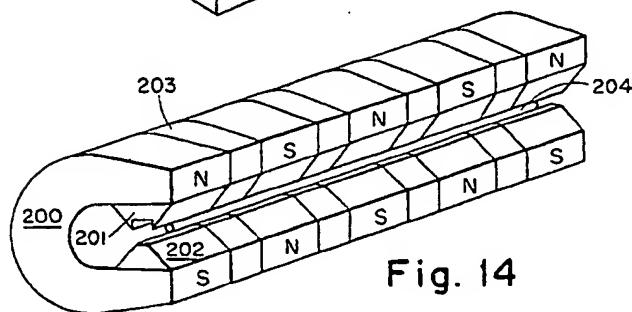


Fig. 14

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COMBINE SPECIFICATION

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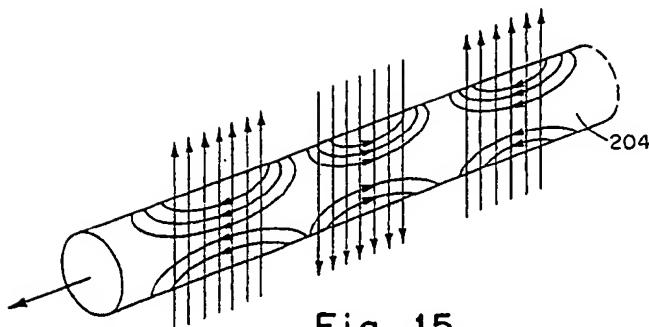


Fig. 15

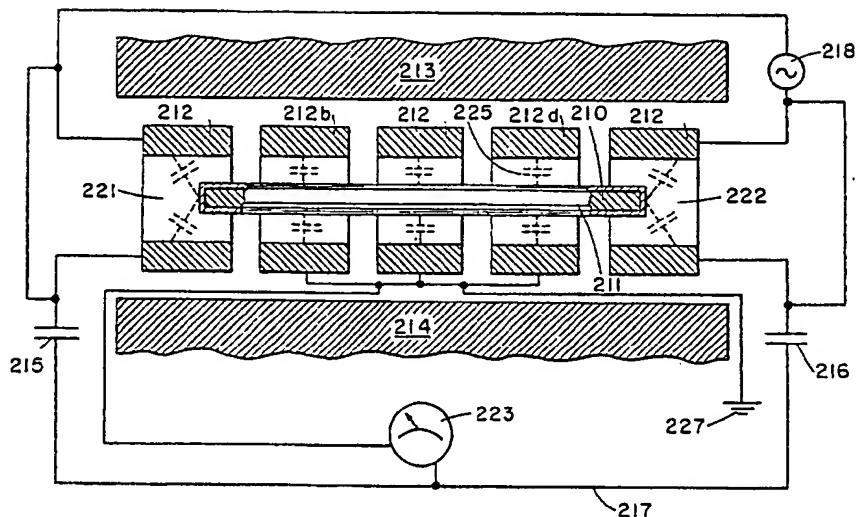


Fig. 16

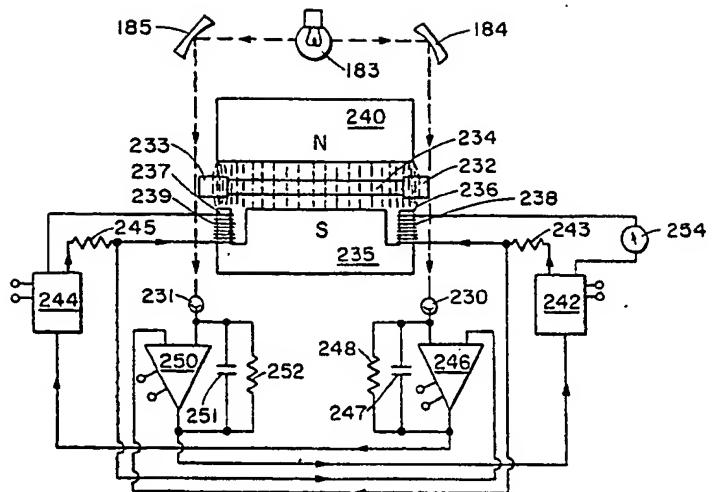


Fig. 17

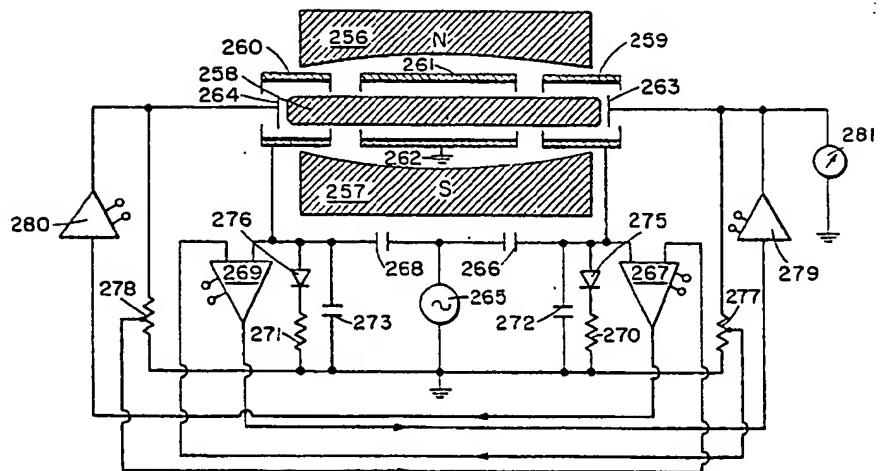


Fig. 18

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